TEST REPORT ON

METAL ROOFING SYSTEMS INC. SYSTEM 2500 ROOF PANELS (24 GA., 2" HIGH, 16" WIDE FLAT PAN PANEL) AT 1' 0" & 5' 0" PURLIN SPACING WITH 180° SEAM IN ACCORDANCE WITH ASTM E1592-05

> TESTED FOR: Metal Roofing Systems, Inc. 7687 Mikron Drive Stanley, NC 28164 Telephone: (704) 820-3110 FAX: (704) 820-0113

TESTED BY: ENCON[®] Technology, Inc. 6717 South Yale Avenue, Suite 200 Tulsa, OK 74136 Telephone: (918) 492-5992 FAX: (918) 493-3568

TEST CONDUCTED AT: ENCON Testing Lab 1216 North Lansing Avenue, Suite C Tulsa, OK 74106

TEST WITNESSED BY: Bala Sockalingam, Ph.D., P.E.

TESTING DATES: May 28 & 29, 2008 REPORTING DATE: May 30, 2008 ENCON[®] Project C1588-1



TABLE OF CONTENTS

SECTION I TEST SUMMARY

1.1	Summary	1
1.2	Roof Description	1
1.3	Test Results	1
1.4	Roof System Details	2-4

SECTION II DESCRIPTION OF TEST

2.1	Description of Test				
	2.1.1	Test Chamber	5		
	2.1.2	Air System	5		
	2.1.3	Deflection and Distortion Measurements	5		
	2.1.4	Test Procedure	5		
	2.1.5	Test Specimen	6		
	2.1.6	Specimen Width and Length	6		
	2.1.7	Specimen Orientation and Sealing	6		
	2.1.8	Failure	7		
2.2	Factor	r of Safety	7		

SECTION III TEST RESULTS

3.1	Specimen Identification	8
3.2	Test Results for 5' 0'' span	9-11
3.3	Test Results for 1' 0'' span	12-14

SECTION IV TEST PHOTOGRAPHS

4.1	Test Photographs	15-19
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SECTION V APPENDIX

5.1	Test Drawings	20-25
5.2	Yield Stress	26
5.3	Test Conditions	27-28

TEST SUMMARY

1.1 SUMMARY

Tests were conducted on Metal Roofing Systems' System 2500 (2" high seam, 16" wide, 24 Ga., 50 ksi) standing seam metal roof panels at ENCON[®] Technology, Inc.'s Test Facility, Tulsa, Oklahoma. These tests meet the provisions of ASTM E 1592-05 and were run for different purlin spacing. The tests are listed below according to their configurations and date tested.

- Test #1: 16" wide, 24 ga. System 2500 panel at 5' 0" purlin spacing with 180° seam. Tested on May 28, 2008.
- Test #2: 16" wide, 24 ga. System 2500 panel at 1'0" purlin spacing with 180° seam. Tested on May 29, 2008.

The above defined tests were witnessed by Bala Sockalingam, Ph.D., P.E., of ENCON Technology.

1.2 ROOF SYSTEM DESCRIPTION

1

2

Metal Roofing's System 2500 roof system consisted of 16" wide, 24 ga., 50 ksi (nom.) yield panels joined together at the sidelaps to form a flat pan profile with a 2" high seam. The panels are attached to the 16 ga. (nom) purlins at 5' 0" & 1' 0" spacing with two piece sliding clips and (2) #10-16 self-drilling screws per clip. The panel sidelaps were mechanically seamed to form a 180° seam.

1.3 TEST RESULTS

The panels were loaded to a failure condition and observations made. In both tests, the failure mode was the bending failure of the clip base. The ultimate and design loads for all tests are shown on Table 1.

40.2

180.5

20.1

90.3

Test	Purlin Spacing	Ultimate Load	Design Load
		(psf)	(psf)

 Table 1. Test Results for 16'' wide, 24 ga. System 2500 Panel

5' 0"

1' 0"

Notes:

- 1. The design load is calculated by dividing the ultimate load by the factor of safety of 2.
- 2. The design loads have not been increased by 33% for wind load.







2.1 DESCRIPTION OF TEST

Tests were conducted to determine the structural performance of the SSMR Panel at various span configurations under uniform static pressure difference. The test method consisted of the following: (1) sealing the test specimen against one face of a test chamber; (2) supplying air to and exhausting air from the chamber at the rate required to maintain the test pressure difference across the specimen; and (3) observing, measuring, and recording the deflections, deformations, and nature of any failures of principal or critical elements of the panel profile or members of the anchor system.

The increments of load application were chosen such that a sufficient number of readings were obtained to determine the load deformation curve of the system. End and edge restraint was representative of field conditions, and the unit contained sufficient individual components to minimize the effect of variations in material and workmanship.

2.1.1 TEST CHAMBER

The test chamber consisted of a box as shown in the applicable drawings in Section V. It contains one open surface against which the test specimen is installed. Two static pressure taps are located at corners to measure the chamber pressure in such a manner that the readings are not affected by the velocity of the air supply to or from the chamber or other air movement. The air supply openings into the chamber are arranged so that the air does not impinge directly on the test specimen with significant velocity.

2.1.2 AIR SYSTEM

The compressed air supply consists of a number of individual compressor units capable of maintaining a constant air pressure difference for the required test period. A digital manometer is used to measure the test pressure difference with accuracy of 1/10".

2.1.3 DEFLECTION AND DISTORTION MEASUREMENT

Deflection and distortion measurements were taken by means of a level and staffs calibrated to 1/100 of an inch, which were attached to the topside of the specimen. The deflection staffs were placed so that movement of the support members did not influence their readings. Reading locations are as shown on the drawings in Section V.

2.1.4 TEST PROCEDURE

A nominal air pressure of 7.8 psf, which was equivalent to four times the dead weight of the specimen, was applied to the test panel for at least a minimum of 60 seconds and until the panel had stabilized and readings were taken. These readings were considered as bench mark readings and the load corresponding to these readings were considered as "Reference Zero Load."

The air pressure was then increased by load increments as shown on recorded data and held for 60 seconds and until the panel had stabilized and the first set of readings were measured for the test panel. The air pressure was then reduced to zero or no load and then once again to the Reference

Zero Load and the bench mark readings were taken.

This procedure was repeated several times each time increasing the air pressure by a load increment over the previous load. It was ensured that benchmark readings were taken between each incremental increase in order to keep track of permanent deflections. This load sequence was continued until the panel was subjected to maximum air pressure resulting in its failure.

2.1.5 TEST SPECIMEN

The test specimen was of sufficient size to determine the performance of all typical parts of the roof system excluding support elements such as purlins, eave struts, rake angles and similar structural parts supporting the roof system. Conditions of structural support of the roof specimen were simulated as accurately as possible. The test specimen included roof panels, concealed anchor clips and perimeter attachment of the roof to its structural supports. All of the parts of the test specimen were actual size and material. The overall dimension of the specimen was $7.75' \times 25.0'$ for 5' 0'' span test and $7.75' \times 10.0'$ for 1' 0'' span test. The panels were supported by secondary structures (purlins). The details of methods of construction and anchorage are depicted in the enclosed test drawings

At the discontinuous end of test panel representing the building "cut side" (Detail 1/6), the only attachment to the underlying purlin was the panel clip. This "cut side" was constructed as if an actual building panel was physically severed into two pieces leaving the test edge of the panel discontinuous in a substantially unsupported condition. Endwall edges "cut end" (Details 1/3 and 1/4) were attached to rake angles or other structural elements by clamps. One eave/sidewall (Detail 1/5) and the panels in the main field of the test setup including the panel clips and its attachment to the secondary structure (purlins) were constructed similar to the panel mounting system that would be used to mount the panel to an actual building structure.

The panel clip is hooked to the male lip of the panel and is attached to the purlin. See Drawings 1/1 and 1/2 for typical location of panel clips and Drawings 1/3 and 1/4 for locations of the panel clip relative to the various edge conditions. Plastic sheeting (max 6 mil thick) was used to keep the air pressure chamber airtight. The sheeting was placed between the purlins and panels. The sheeting between panel clips was pleated to allow the sheeting to flow into the panel sidelap when air pressure was applied to the panels.

2.1.6 SPECIMEN WIDTH & LENGTH

The specimen width contained no less than five full panels and five structural elements. Edge seals did not constrain the specimen any more than normal gable attachment. With two ends crosswise restraint, the panels spanned 5 equal spans of 5' 0". With only one end crosswise restraint, the panels spanned 10 equal spans of 1' 0".

2.1.7 SPECIMEN ORIENTATION AND SEALING

The test specimen was installed in its "as used" orientation, i.e., the interior side of the specimen faced the applied air pressure. The panel was secured to the test jig by the same number and type of

concealed anchor clips as are normally used for installation of the test specimen on a building. The use of tape or film did not restrict differential movement between adjoining members.

2.1.8 FAILURE

Failure was considered to have occurred when components separated or permanent distortion interfered with the function of the system or the system was unable to carry additional load. Permanent deformation of the panel across the flat (area between the ribs) which does not adversely affect roof watertightness or roof performance was not considered failure.

2.2 FACTOR OF SAFETY

The design loads was calculated with factor of safety of 2 as per AISI-NAS 2001 Specifications and 2004 Supplement.

3.1 SPECIMEN IDENTIFICATION

Manufacturer:	Metal Roofing Systems
Model Type:	System 2500 Panel
Dimensions:	2" high seam, 16" wide flat pan profile with 180° seam
Panel Gauge:	24 ga.
Base Metal Thickness:	0.020"
Panel Yield Strength:	53.5 ksi
Elongation in 2":	24 %
Panel Coating:	Painted Finish
Clip Type:	System 2500 two piece sliding clip
Clip Material:	Clip tab - 0.030" thick, 1.75" wide Clip base - 0.044" thick, 5.0" wide
Fasteners:	(2) #10-16 SDS
Purlin:	16 ga. (0.058" thick)

Note: All the test materials were supplied by Metal Roofing Systems and were not sampled by ENCON.

3.2 TEST RESULTS FOR 16" WIDE, 24 GA. PANELS AT 5' 0" PURLIN SPACING

Testing of 24 Ga., Metal Roofing Systems System 2500 Panel @ 5'-0" Purlin Spacing with 180° Seam

No.	Pressure	Time		Deflection (in)					
	psf	Sec	1	2	3	4	5	6	Remarks
1	15.6	60.0	0.09	0.67	0.14	0.89	0.12	0.13	
2	7.8		0.05	0.05	0.07	0.06	0.07	-0.03	
3	26.0	60.0	0.24	1.65	0.27	2.18	0.24	1.69	
4	7.8		0.13	-0.02	0.12	0.24	0.11	-0.09	
5	31.2	60.0	0.67	2.35	0.71	3.00	0.56	2.44	
6	7.8		0.39	1.86	0.42	2.41	0.32	1.83	
7	36.4	60.0	1.04	2.91	1.07	3.49	0.89	2.96	
8	7.8		0.85	2.24	0.81	2.73	0.64	2.09	
9	40.2	0.0							

Air Pressure Test #1 Conducted On May 28, 2008

Failure Mode:

Bending failure of clip base



Load vs Panel Flat Deflections 5' 0'' Span (24 ga.) with 180° Seam

Note: P Set denotes permanent deflection after each load cycle.



Load vs Panel Rib Deflections 5' 0'' Span (24 ga.) with 180° Seam

Note: P Set denotes permanent deflection after each load cycle.

3.3 TEST RESULTS FOR 16" WIDE, 24 GA. PANELS AT 1' 0" PURLIN SPACING

Testing of 24 Ga., Metal Roofing Systems System 2500 Panel @ 1'-0" Purlin Spacing with 180° Seam

No.	Pressure	Time		Deflection (in)					
	psf	Sec	1	2	3	4	5	6	Remarks
1	62.4	60.0	0.13	2.42	0.15	2.69	0.14	2.96	
2	7.8		0.03	0.66	0.02	0.77	0.03	0.89	
3	93.6	60.0	0.27	3.39	0.34	3.76	0.37	4.16	
4	7.8		0.04	2.11	0.07	2.45	0.09	2.78	
5	124.8	60.0	0.48	4.21	0.61	4.71	0.70	5.17	
6	7.8		0.27	2.87	0.34	3.35	0.38	3.84	
7	156.0	60.0	0.75	4.99	0.95	5.57	1.08	6.12	
8	7.8		0.45	3.71	0.55	4.30	0.63	4.88	
9	180.5	0.0							

Air Pressure Test #2 Conducted On May 29, 2008

Failure Mode:

Bending failure of clip base



Load vs Panel Flat Deflections 1' 0'' Span (24 ga.) with 180° Seam

Note: P Set denotes permanent deflection after each load cycle.



Load vs Panel Rib Deflections 1' 0'' Span (24 ga.) with 180° Seam

Note: P Set denotes permanent deflection after each load cycle.



RESTRAINT END



5

5'0"

1

1

PLAN VIEW OF TEST ROOF

PURLIN SPACING













Sherry Laboratories 3100 North Hemlock Circle Broken Arrow, OK 74012-1115

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Report No.:

P.O. No.:

Date Received:

Date Reported:

08051019-001-v1

5/28/2008

5/29/2008

Verbal

Tel: 918-258-6066 800-982-8378 Fax: 918-258-1154

LABORATORY REPORT

Attn: Bala Sockalingam ENCON Technology, Inc. 6717 S. Yale Ave., Suite 200 Tulsa, OK 74136-3327

Sample Description: System 2500 Panel

Tensile Test (Rectangular) per ASTM E8-08

Parameter	Result	815
Thickness, inch	0.020	
Width, inch	0.503	
Tensile Strength, psi	62,000	
Yield Strength, psi at 0.2% offset	53,500	
Elongation in 2 inches, %	24	

Approved by:

Jeffrey Simmons, Laboratory Director Sherry Laboratories

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APPENDIX

5.3 TEST CONDITIONS

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APPENDIX

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ENCON[®] TECHNOLOGY, INC., 2008

TEST REPORT ON

METAL ROOFING SYSTEMS INC. SYSTEM 2500 ROOF PANELS (24 GA., 2" HIGH, 16" WIDE FLAT PAN PANEL) AT 5' 0" – 3' 9" PANEL SPANS IN ACCORDANCE WITH ASTM E1646-95 (2003) & E1680-95 (2003)

> TESTED FOR: Metal Roofing Systems, Inc. 7687 Mikron Drive Stanley, NC 28164 Telephone: (704) 820-3110 FAX: (704) 820-0113

TESTED BY: ENCON[®] Technology, Inc. 6717 South Yale Avenue, Suite 200 Tulsa, OK 74136 Telephone: (918) 492-5992 FAX: (918) 493-3568

TEST CONDUCTED AT: ENCON Testing Lab 1216 North Lansing Avenue, Suite C Tulsa, OK 74106

TEST WITNESSED BY: Bala Sockalingam, Ph.D., P.E.

TESTING DATE: May 30, 2008 REPORTING DATE: May 31, 2008 ENCON[®] Project C1589-1



TABLE OF CONTENTS

SECTION I	TES	T SUMMARY	Page Number
	1.1	Summary	1
		Panel System Description	1
		Test Results	1-2
	1.4	Test Panel	3
SECTION II	DES	CRIPTION OF TEST	
	2.1	Description of Test	4-5
SECTION III	TES	T RESULTS	
	3.1	Specimen Identification	6
	3.2	Test Data	7
SECTION IV	TES	T PHOTOGRAPHS	
	4.1	Test Photographs	8-12
SECTION V	APP	ENDIX	
	5.1	Test Drawings	13-14
	5.2	Flowmeter Calibration Chart	15
	5.3	Test Conditions	16-17

TEST SUMMARY

1.1 SUMMARY

Tests were conducted on Metal Roofing Systems' System 2500 (2" high seam, 16" wide, 24 Ga., 50 ksi) standing seam metal roof panels at ENCON® Technology, Inc.'s Test Facility, Tulsa, Oklahoma. The purpose of the tests was to determine the resistance of exterior metal roof panel system with sealant to water penetration and air infiltration resulting from static air pressure difference between the exterior and interior surfaces. These tests meet the provisions of ASTM E1680-95 (2003) "Standard Test Method for Rate of Air Leakage Through Exterior Metal Roof Panel Systems" and ASTM E1646-95 (2003) "Standard Test Method for Water Penetration of Exterior Metal Roof Panel Systems by Uniform Static Air Pressure Difference".

The above-defined tests were witnessed by Bala Sockalingam, Ph.D., P.E., of ENCON Technology Inc. The panels were installed on May 28, 2008 and tested on May 30, 2008.

1.2 PANEL SYSTEM DESCRIPTION

Metal Roofing's System 2500 roof system consisted of 16" wide, 24 ga., 50 ksi (nom.) yield panels joined together at the sidelaps to form a flat pan profile with a 2" high seam as shown on Page 2.

The sidelap sealant used in these panels was Q'So Inc.'s Q-54 Mastomeric Butyl Sealant. The nominal diameter of the sealant bead was 3/16". The System 2500 panels were attached to nominal 16 ga., 6" deep, Cee purlin with two piece sliding clips and (2) #10-16 self-drilling screws per clip. Each panel spanned over unequal spans of 5' 0" and 3' 9". The panel sidelaps were mechanically seamed to form a 180° panel seam.

1.3 TEST RESULTS

The panel system was preloaded for positive and negative load of 15 psf. The panel sidelaps were sealed to measure the extraneous leakage of the test chamber and test specimen perimeter. The panel sidelaps were unsealed and the air leakage rates were then measured for static positive pressure difference of 1.57, 6.24 & 12.0 psf. Upon completion of the air leakage test, the panel system was uniformly sprayed with water at a rate of 5.0 gal/ft² per hour for 15 minutes at a static positive (inward) pressure difference of 12.0 psf. The results for the two tests are summarized on Page 2.



- 3. PANELS SPANNED TWO UNEQUAL SPANS OF 5' 0" AND 3' 9".
- 4. 3/16" BEAD SEALANT WAS FACTORY APPLIED IN THE PANEL SEAM.



2.1 DESCRIPTION OF TEST

OBJECTIVES

The purpose of the tests was to determine the resistance of metal roof panel systems to water penetration and air infiltration resulting from static air pressure difference between the exterior and interior surfaces. The test method consisted of the following:

- 1. assembling the test panel in the test chamber to form a typical roof construction;
- 2. measuring the air leakage through the panel sidelaps and extraneous leakage of the test chambers;
- 3. spraying the exterior roof surface with water to determine any water penetration through panel sidelaps

TEST CHAMBER

The test chamber consisted of a box as shown in the applicable drawings in Section V. It contains one open surface against which the test specimen was installed. One static pressure tap is located at a corner to measure the chamber pressure in such a manner that the reading was not affected by the velocity of the air supply to or from the chamber or other air movement. The air supply opening into the chamber was arranged so that the air does not impinge directly on the test specimen with significant velocity.

AIR SYSTEM

The compressed air supply consists of a compressor unit capable of maintaining a constant positive or negative air pressure difference for the required test period. A digital manometer was used to measure the test pressure difference with accuracy of 1/100."

AIR FLOW METERING SYSTEM

A laminar flow element capable of measuring airflow of 40 SCFM was used to measure the air leakage through the panel sidelaps and extraneous leakage of the test chambers. The flow was measured as a differential pressure using a digital manometer and converted to actual flow using regression equation shown on the flowmeter calibration chart.

WATER SPRAY SYSTEM

The water spray system consists of equally spaced nozzles located at a uniform distance from the test specimen. The system was calibrated to deliver a minimum rate of 5.0 gal/ft^2 per hour.

CALIBRATION

The water spray was calibrated on April 24, 2008 and the air-flow measuring system was calibrated on February 13, 2008.

TEST SPECIMEN

The overall dimension of the test construction was in excess of 7' 9" x 8' 9". The panels covered unequal spans of 5' 0" and 3' 9". The construction width contained four full panels and two partial panels. The panels were attached to an intermediate Cee purlin section with panel clips and (2) #10-16 self-drilling screws per clip. The panels were attached to 16 ga. eave, rake and ridge sections with self-drilling screws. An overflow device that provided a $\frac{1}{2}$ " to $\frac{3}{4}$ " deep water pond was installed on one end of the test specimen. The perimeter of the test construction was sealed to the test chamber wall. The perimeter seals between the panels and the test chamber did not duplicate the actual building perimeter details. The details of the methods of construction are depicted in the enclosed test drawings in Section V.

TEST PROCEDURE

The support beams were moved to 75% of the design thermal movement of the panel clip to the support. This operation was conducted once for a total of two cycles. All supports beam connections to the test chamber were tightened.

The test specimen was preloaded to a positive load greater than or equal to 15 psf or 75% of the building live load or 50 % of the design positive wind pressure difference. The test specimen was also preloaded to a negative load greater than or equal to 50 % of the building design wind uplift pressure difference.

The panel sidelap was temporarily sealed to measure the extraneous air leakage, Q_L , of the test chamber for the specified test pressure difference across the test specimen. The temporary sidelap seal was removed and the airflow through the sidelaps was measured after the test conditions were stabilized for the specified test pressure difference across the test specimen. This measured airflow was designated the total metered airflow, Q_M . The air leakage, Q, through the test specimen was equal to $Q_M - Q_L$. The ambient room temperature at the test specimen was also measured.

Upon the completion of the air leakage test, the water spray system was installed over the test specimen. The test specimen was subjected to the specified positive (inward) test pressure difference for 15 minutes while the spray system delivered water on the test specimen at a rate of 5.0 gal/ft² per hour. The depth and the temperature of the ponded water on the test surface were measured. The test specimen was observed for possible water leakage.

3.1 SPECIMEN IDENTIFICATION

Manufacturer:	Metal Roofing Systems
Model Type:	System 2500 Panel
Dimensions:	2" high seam, 16" wide flat pan profile with 180° seam
Panel Gauge:	24
Clip Type:	System 2500 two piece sliding clip
Fasteners:	(2) #10-16 SDS
Purlin:	16 ga. (0.059" thick)
Sealant Manufacturer:	Q'So Inc.
Panel Sealant:	Q-54 Mastomeric Butyl Sealant
Sealant Size:	Nom. 3/16" bead
Thermal Movement:	±0.625"

Note: All the test materials were supplied by Metal Roofing Systems and were not sampled by ENCON.

3.2 TEST DATA

Date:	5.30.2008
Panel Manufacturer	Metal Roofing Systems
Panel Type	System 2500
Panel Gauge	24
Panel Width (in)	16
Panel Attachment	System 2500 Clip with (2) #10-16 SDS
Sealant Manufacturer	Q'So Inc.
Panel Sealant	Q-54 Mastomeric Butyl Sealant (Nom. 3/16" Bead)
Panel Span (ft)	5' 0" - 3' 9"
Test Area (ft ²)	67.8
Preload Positive Pressure (psf)	15
Preload Negative Pressure (psf)	15
Ambient Temperature (F)	78.8
Panel Temperature (F)	78.2
Barometric Pressure (in. Hg)	29.15
Water Depth (in)	0.625

Test Method: ASTM E1680-95 (2003)

Test	Static Pressure	Initial	Initial	Final	Final	Total Air	Air Infi	iltration
No.	Difference	Reading	Reading ¹	Reading	Reading ¹	Leakage ²	Ra	nte
	psf	DP (in)	cfm	DP (in)	cfm	cfm	cfm/ft ²	cfm/lin.ft
1	1.57	0.861	4.411	0.867	4.442	0.0300	0.0004	0.0006
2	6.24	2.251	11.501	2.261	11.552	0.0497	0.0007	0.0010
3	12.00	3.456	17.615	3.472	17.696	0.0792	0.0012	0.0016

 1 The actual flow is calculated using the regression equation shown on the flowmeter calibration chart.

² Total Air Leakage $Q_{st} = Q x (1.326 x B / (0.075 x (T + 460)))^{0.5}$

Test Method: ASTM E1646-95 (2003)

I	Test	Static Pressure	Rate	Test	Water Infiltration
	No.	Difference	(gal/hr/ft ²)	Duration	
		psf		(min)	
	1	12	5	15	No Water Leakage



SYSTEM 2500 PANELS TEST DETAILS

ASTM E1646 & E1680 13/17







14/17

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15555 North 79th Place Scottsdale, AZ 85260 Phone: (480) 948-3789 Fax: (480) 948-3610 www.flow-dynamics.com sales@flow-dynamics.com

Calibration Report

Customer Name:	Encon Technology,Inc.	Report #	FCAL10825-784180-R1
Customer Address:	6717 South Yale Ave., Suite 200, Tul	sa, OK 74136	
Customer PO #	CC	Received Date:	7/19/2006
Model #	50MW20-2	Cal Date:	8/3/2007
Serial #	784180-R1	Meter Type:	LFE
Lab Temp :	77 Deg F	Fluid Type:	Air
Calibration Procedure:	FDP-001	Lab Relative Humidity	: 38%
		Calibration Tech:	P. Del Ferraro
Notes, Adjustments	STP: 70F & 14.7 PSIA		

Notes, AdjustmentsSTP: 70F & 14.7 PSIAand Repairs :Pressure measured at Inlet

Calibration Results (As Found = As Left)

Test Point	Meter Pres	Delta P	Meter Temp	Act. Flow	Std. Flow	C Factor	K Factor	Viscosity
#	PSIA	In H20 @4C	Deg. F	ACFM	SCFM	Rho*dP/mu^2	Q*mu/dP	mP
1	15.261	8.1828	74.7658	41.5958	42.8084	1.8633E-05	935.271	184.01
2	15.109	7.4473	75.5311	38.0853	38.7507	1.6724E-05	942.061	184.24
3	15.045	7.1836	75.6097	36.8346	37.3144	1.6057E-05	944.686	184.27
4	14.860	6.1442	75.3245	31.8309	31.8658	1.3585E-05	954.017	184.18
5	14.709	5,1714	75.3997	27.0360	26.7865	1.1314E-05	962.844	184.20
6	14.553	4.0788	75.2852	21.5180	21.0983	8.8341E-06	971.424	184.16
7	14.435	3.0788	75.4941	16.3684	15.9127	6.6072E-06	979.281	184.23
8	14.372	2.5054	75.4786	13.3806	12.9516	5.3536E-06	983.710	184.22
9	14.285	1.4896	75.4576	8.01385	7.71028	3.1641E-06	990.888	184.21
10	14.249	0.9949	75.4228	5.37050	5.15437	2.1084E-06	994.176	184.20
11	14.232	0.7306	75.3947	3.95135	3.78801	1.5466E-06	996.033	184.19
12	14.216	0.4667	75.2987	2.52765	2.42087	9.8736E-07	997.287	184.17

Standards Used in Calibration

Standard #	Description	Serial #	ReCal Date
FDI 05	5 Cu. Ft. Bell, 1 cuft volumes	N/A	1/08/2008
FDI 123	Bell Computer Cart (A/D; Volts, mA, Temp.)	N/A	2/19/2008
FDI 24	Heise Press Trans 150 PSIA	S9-21856	1/10/2008
FDI 101	Digital Pressure Gauge	531887	5/23/2008
FDI 44	Diff Press Trans 10" H2O	241130	8/5/2007

The instrument referenced above was calibrated using standards traceable to the National Institute of Standards and Technology. Calibration reports for references maintained by FDI are available upon request to the customer of this calibration report. The volumetric flowrates reported are within a best uncertainty of +/- 0.2% of reading. Flow Dynamics, Inc. calibration services comply with ANSI Z540-1-1994, ISO Guide 25 and ISO 9001:2000 and accredited to NVLAP NIST Handbook 150 and ISO/IEC 17025:2005.

The results reported relate only to the item(s) calibrated as described above. This report may not be reproduced, except in full, without the written approval of Flow Dynamics Inc.

I certify the accuracy of this Calibration Report:

Andrew Yee Name

Calibration Engineer Title

Signature



APPENDIX

5.3 TEST CONDITIONS

A. OWNERSHIP OF ENCON WORK PRODUCT

All test results developed as a part of this work shall be CUSTOMER's property. All samples submitted to ENCON for testing shall become the property of ENCON. CUSTOMER understands that any test program including procedures and test machines incorporated as a part of this work is a result of continuing long-term research and development by ENCON and because of this all ENCON test procedures, test drawings and other intellectual property relating to this work is and shall remain the property of ENCON. Test samples were disposed of shortly after completion of the tests unless other arrangements were agreed to in writing prior to the test.

ENCON will use its normal procedures to retain copies of the information developed as a part of this test for a period of three years from the date the work was done. This material may be routinely destroyed thereafter.

B. ENCON GUARANTEE

ENCON guarantees it used its best effort to accomplish this test work. Work done by ENCON was carefully completed by personnel believed to be competent. ENCON tests were based on what was currently believed to be good engineering practices in use at the time of the test.

The safety factors used are generally accepted as suitable to produce safe results. However, good engineering practices and applicable codes and insurance requirements must be taken into consideration in determining if a test procedure is satisfactory for a specific end use. Applicable specifications, good engineering practices and applicable safety factors may change in the future. CUSTOMER should be alert to these changes.

The information and test results presented by ENCON in this test report are offered in good faith based on information ENCON believes to be reliable. This information is offered as a guide to assist CUSTOMER in CUSTOMER's endeavors and does not contain any warranties as to fitness by ENCON. No REPRESENTATION OF WARRANTIES, EXPRESS OR IMPLIED, INCLUDING THOSE OF MERCHANTABILITY AND OF FITNESS FOR A PARTICULAR PURPOSE are made by ENCON, and more specifically, ENCON hereby expressly disclaim such. In no event shall ENCON be liable for ANY CONSEQUENTIAL, INCIDENTAL OR SPECIAL DAMAGES, including, without limitation, labor, transportation, loss of use, loss of profits, harm, personnel injury and damage to property.

If any doubt exists as to the proper means of interpreting or using the test results contained herein, contact ENCON for clarification. CUSTOMER should assure themselves through careful evaluations that test results are suitable for those end uses to which CUSTOMER intends to put them.

APPENDIX

Information and material provided by CUSTOMER to ENCON was reviewed by an ENCON executive. However, ENCON does not accept the responsibility for accuracy or verification of CUSTOMER's information or the suitability of CUSTOMER materials. Materials supplied by CUSTOMER were tested as received and were not evaluated for code or insurance compliance. CUSTOMER is expected to review the ENCON drawings, tables, test results and other information provided by ENCON to CUSTOMER critically so as to assure CUSTOMER that these presentations, formulas, drawings and other information are accurate and meaningful for the purpose intended.

No other warranties or guarantees shall be issued, implied, delivered or otherwise construed to be issued, implied or delivered.

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